Adaptive Steam Temperature Regulation for Essential Oil Extraction Process

Mazidah Tajjudin¹*, Mohd Hezri Fazalul Rahiman¹, Norlela Ishak¹, Hashimah Ismail², Norhashim Mohd Arshad¹, Ramli Adnan¹

¹Faculty of Electrical Engineering, University Teknologi MARA, 40450, Shah Alam, Selangor, Malaysia
²Faculty of Engineering, University Selangor, 40450, Bestari Jaya, Selangor, Malaysia

Abstract Essential oil is volatile and sensitive to excessive heat. Many studies had shown that temperature during extraction process had a great impact on the oil quality. Despite of that, until now there are very few research had been published on the control development of essential oil extraction system. Hence, this study was commenced particularly on the development of a regulated essential oil extraction system using self-tuning control. A self-tuning control was applied using pole-assignment method to regulate the steam temperature throughout the extraction process. Combination of controller poles in real and imaginary axis may influence the closed-loop response so that the steam can reach the set point faster but yet with minimal overshoot. Extensive analysis was done by simulation in order to understand the effect of the poles location and also the selection of sampling time over the closed-loop response. Outcome from the simulation was applied on the real process where the controller produced satisfactory result as expected. The controller was able to regulate the steam temperature at a desired level and maintained within ±2% output boundary.

Keywords Self-Tuning PID, Steam Distillation, Essential Oil Extraction, Pole-Assignment, Recursive Least Square

1. Introduction

Steam distillation is among the most popular method for essential oil extraction process. The proportion of different essential oils extracted by steam distillation is 93% and the remaining 7% is extracted by other methods such as hydro distillation[1]. This method applies hot steam to extract the essential oil from the raw materials. The mixture of oil and steam will be condensed and separated at their liquid form. In the majority of cases the oil is less dense than water and so forms the top layer of the distillate and can be separated easily using proper method and instruments.

Continual exposure to excessive heat may degrade the quality of the essential oil as had been studied and reported in[2] for ginger extraction. The study proposed that steam temperature needs to be regulated below saturated temperature throughout the extraction process. This finding had been supported by lots of other published works[3–7]. Nevertheless, there were very few literature on the control development for extraction system was found.

This study initiates the development of an automated essential oil extraction system using steam distillation technique. The system was able to perform steam distillation at a regulated temperature up to 100°C.

Steam temperature control had been studied and applied using various methods. Most of the publications focused on the superheated steam temperature control. There is very little publication so far that discussed on the steam temperature regulation below 100°C. Nonetheless, other studies pointed out the same non trivial issues in steam temperature regulation which is normally comes from the nonlinearity, slow varying process dynamics, fast disturbance and unmodeled dynamics[8–11]. Dynamics of the process may be changed due to load variations and sometimes from unpredictable causes. These attributes made fixed parameter controller such as PID is inefficient to perform satisfactory control for steam temperature.

It is not doubtful that PID controllers are still widely used in industries nowadays despite of the advancement in process control technology. It has been reported that more than 97% of the controllers in process control industries are of PID type[12]. The ability of PID control mode to compensate most practical industrial processes has led to their wide acceptance such as in pulp and paper industries. In addition, it simple structure and easy to understand has made tuning procedures more easy to comprehend and can be accomplished by trial and error by technical personnel. Furthermore, the presence of integral term will ensure zero steady-state error for a step change in input signal.
Nevertheless, PID controller will only performed well within limited operating range where tuning was performed unless the process is linear. Unfortunately, even though the control structure seems simple, there were no generic tuning procedures that can sustain satisfactory performance over variation of process types. This drawback has led to continual research in PID control leading to different kind of tuning approaches. Some of the renowned methods applying phase margin and gain margin, the internal mode control (IMC) design method, direct synthesis method, graphical technique, optimization technique, and frequency response analysis[13]. An extensive summary of some well-known PID tuning techniques can be found in[14]and[15].

An adaptive PID or the self-tuning PID on the other hand will automatically adjust the controller parameters based on the control laws. This control scheme is attractive especially if there is only little information about the process to be controlled is known. In fact, there are lot of on-going research in refining the algorithms to tailor the needs of specific applications[16].

This paper focused on applying the self-tuning PID to regulate steam temperature in steam distillation process for essential oil extraction. Steam distillation process possessed a slow varying dynamics with varying time-delay and process gain over its full-range. Specific operating range need to be identified where the control can be accomplished successfully. The process was described by autoregressive with exogeneous input (ARX). The unknown parameters were updated using Recursive Least Square (RLS) method while controller design was based on pole placement.

An overview about steam distillation for essential oil extraction process was discussed in Section 2. Section 3 explained on the self-tuning control design and algorithm using pole-placement method. Some simulation results to show the effect of poles selection will be discussed in section 4. The simulation will then be verified with experimental evaluation in section 5.

2. Steam Distillation Essential Oil Extraction Process

A pilot-scale steam distillation plant developed for this study consists of a stainless steel column of 26 cm inner diameter and a vertically mounted steel condenser to convert the steam into liquid form. Figure 1 shows the simplified schematic diagram of the plant. Two RTDs were installed; RTD1 was immersed in the water to monitor water temperature while RTD2 was installed 40cm from RTD1 to monitor the steam temperature inside the column. The distance of the sensor from its heat source will caused transport delay in steam temperature measurement.

During operation, steam will be generated by boiling the water inside the distillation column. In normal operation, the water volume is 6 litres. The water was heated up by a 1.5kW coil-type heater. It took about 3500s to boil the water. The open-loop response under normal operating condition is shown in Figure 2. Column temperature that represents the steam temperature started to rise gradually after 1500s when water temperature is around 70°C. The steam temperature increased exponentially until 80°C where the steam rate hiked to 100°C and saturates. During this state, temperature within the column is at homogeneous.

The objective of this research is to regulate the steam temperature below 100°C as to preserve the oil from burning and consequently preserving its quality. During closed-loop operation, the steam temperature will be measured by RTD2. RTD2 was installed over the raw material to monitor the temperature of steam that passed through the raw material instead of measuring the steam temperature that will enter the raw material bed.

Some signal conversion needs to be done to convert the resistance from RTD to voltage signal that was compatible with the acquisition card PCI 1711. The signal converter converts 0°C to 120°C to 1V to 5V. This signal was the measured variable of the process. Control signal from the controller manipulated the heater power by providing a d.c voltage from 0V to 5V to a continuous power controller.

Figure 1. Steam distillation for essential oil extraction diagram

Figure 2. Open loop response of water and steam temperature

From the open-loop response, the model was identified within its linear operating temperature of 80°C to 100°C. The process was fitted to a second-order system using
System Identification Toolbox and fine-tuned to minimize the residual from experimental data. The best fit model was
given by equation (3).

\[ G(s) = \frac{0.000366}{(s+0.011)(s+0.0074)} \]  

(3)

The process gain for the specified range is 4.5°C/V. Comparison between experimental data and the predicted model output gives RMSE of 0.042°C.

3. Self-tuning Pole Placement

Self-tuning control (STC) contains two algorithms; one for the online parameter estimation and the other is for control law implementation. This method uses the information from model parameters that must be updated recursively in order to synthesize a new control system. A self-tuning controller, the recursive process estimation was not necessary. This type of controller is referred to as implicit self-tuning controller.

Most of the explicit STCs apply certainty equivalence principle where model uncertainties during parameter estimation were not considered. It is assumed that these values correspond to their actual values. Theoretical details of the principal can be found in prominent textbooks of adaptive control[16][17]. Figure 3 shows a block diagram of an explicit self-tuning control structure.

The control structure based on pole-placement method is shown in Figure 4.

For explicit self-tuning control, a parametric model is more appropriate because the plant parameters need to be updated at each sampling interval. For this study, second-order ARX structure had been identified as the most suitable model structure. The process transfer function is given by

\[ B(z^{-1}) = b_1 z^{-1} + b_2 z^{-2} \]

The transfer function of a controller is

\[ G_p(z) = \frac{Y(z)}{E(z)} = \frac{G(z)}{P(z)} \]  

(5)

where \( E(z) = W(z) - Y(z) \) or the closed-loop system error and

\[ P(z^{-1}) = (1 - z^{-1})(1 + Yz^{-1}) \]

\[ Q(z^{-1}) = q_0 + q_1 z^{-1} + q_2 z^{-2} \]

By substituting \( P(z^{-1}) \) and \( Q(z^{-1}) \) into equation (5), the controller output becomes

\[ u(k) = q_0 e(k) + q_1 e(k - 1) + q_2 e(k - 2) + (1 - Y)u(k - 1) + Yu(k - 2) \]  

(6)

\( q_0, q_1, q_2, \) and \( Y \) will be determined according to design specifications. The closed-loop transfer function is then becomes

\[ G(z) = \frac{Y(z)}{W(z)} = \frac{B(z^{-1})Q(z^{-1})}{A(z^{-1})} \]  

(7)

with characteristics polynomial of

\[ A(z^{-1})P(z^{-1}) + B(z^{-1})Q(z^{-1}) = D(z^{-1}) \]  

(8)

where \( D(z^{-1}) \) is the desired characteristics polynomial in the form

\[ D(z^{-1}) = 1 + d_1 z^{-1} + d_2 z^{-2} + d_3 z^{-3} + d_4 z^{-4} \]  

(9)

For easier determination of system overshoot and response speed, the following characteristics polynomial is preferable[19].

\[ D(z^{-1}) = (z - \alpha)^2[z - (\alpha + j\omega)][z - (\alpha - j\omega)] \]  

(10)

The characteristics polynomial in equation (10) has double real poles given by \( \alpha \) and a pair of complex conjugate poles where \( \alpha^2 + \omega^2 < 1 \). Parameter \( \alpha \) influenced the speed of the closed-loop system while \( \omega \) determined the desired overshoot. Equation (8) and (10) give a set of four linear algebraic equations as follows:

\[ q_0 b_1 + \gamma = c + 1 - a_1 \]

\[ q_0 b_2 + q_1 b_1 + \gamma(a_1 - 1) = d + a_1 - a_2 \]  

(11)

\[ q_1 b_2 + q_2 b_1 + \gamma(a_2 - a_1) = f + a_2 \]

\[ q_2 b_2 - \gamma a_2 = g \]

where

\[ c = -4\alpha^2; \ d = 6\alpha^2 + \omega^2 \]

\[ f = -2\alpha(2\alpha^2 + \omega^2); \ g = \alpha^2(\alpha^2 + \omega^2) \]  

(12)

Solving equation (11) will determine the controller parameters.

The ARX regression model in recursive form can be written as

\[ y(k) = \theta^T(k)\varphi(k - 1) + e(k) \]  

(13)

where

\[ \theta^T(k) = [a_1 a_2 ... a_n b_1 b_2 ... b_n] \]

is the parameter vector and

\[ \varphi^T(k - 1) = [-y(k - 1), -y(k - 2), ..., -y(k - na), u(k - 1), u(k - 2), ..., u(k - nb)] \]

is the regression vector. The non-measurable random component \( e(k) \) is assumed to be zero for simplicity. The quality of the regression model is evaluated by the prediction error given by

\[ \hat{e}(k) = y(k) - \hat{y}(k) \]  

(14)

where \( \hat{y}(k) \) is the predicted output.

Parameter vector is therefore can be determined by minimizing the loss function given in equation (15) using the
recursive least square (RLS) algorithm that is widely used and can be referred in [20] and [21] for more detail.

\[ J_k(\theta) = \sum_{t=0}^{k} e^2(t) \]  

(15)

The algorithm had been verified with known parameters ARX model in equation 16.

\[ A(q) = 1 - 1.988 q^{-1} + 0.988 q^{-2} \]

\[ B(q) = 0.006521 q^{-1} - 0.006378 q^{-2} \]  

(16)

Online estimation using the RLS algorithm produced the estimated values given in Table 1. All the estimated values are within acceptable range of deviation.

<table>
<thead>
<tr>
<th>Exp Ts</th>
<th>α</th>
<th>ω</th>
<th>Overshoot (%)</th>
<th>Settling time (s)</th>
</tr>
</thead>
<tbody>
<tr>
<td>A1</td>
<td>10</td>
<td>0.1 0.0</td>
<td>0.67</td>
<td>100</td>
</tr>
<tr>
<td>A2</td>
<td>10</td>
<td>0.1 0.1</td>
<td>0.67</td>
<td>100</td>
</tr>
<tr>
<td>A3</td>
<td>10</td>
<td>0.5 0.1</td>
<td>0</td>
<td>8</td>
</tr>
<tr>
<td>A4</td>
<td>10</td>
<td>0.8 0.1</td>
<td>0</td>
<td>0</td>
</tr>
<tr>
<td>A5</td>
<td>10</td>
<td>0.9 0.1</td>
<td>0</td>
<td>10</td>
</tr>
<tr>
<td>A6</td>
<td>10</td>
<td>0.1 0.5</td>
<td>3.0</td>
<td>110</td>
</tr>
<tr>
<td>A7</td>
<td>10</td>
<td>0.1 0.8</td>
<td>2.7</td>
<td>120</td>
</tr>
<tr>
<td>A8</td>
<td>10</td>
<td>0.1 0.9</td>
<td>3.0</td>
<td>160</td>
</tr>
<tr>
<td>A9</td>
<td>20</td>
<td>0.1 0.0</td>
<td>0</td>
<td>73</td>
</tr>
<tr>
<td>A10</td>
<td>20</td>
<td>0.1 0.1</td>
<td>0</td>
<td>127</td>
</tr>
<tr>
<td>A11</td>
<td>20</td>
<td>0.5 0.1</td>
<td>0</td>
<td>13</td>
</tr>
<tr>
<td>A12</td>
<td>20</td>
<td>0.8 0.1</td>
<td>0</td>
<td>5</td>
</tr>
<tr>
<td>A13</td>
<td>20</td>
<td>0.9 0.1</td>
<td>osc</td>
<td>osc</td>
</tr>
<tr>
<td>A14</td>
<td>20</td>
<td>0.1 0.5</td>
<td>osc</td>
<td>osc</td>
</tr>
<tr>
<td>A15</td>
<td>20</td>
<td>0.1 0.8</td>
<td>3.0</td>
<td>450</td>
</tr>
<tr>
<td>A16</td>
<td>20</td>
<td>0.1 0.9</td>
<td>5.0</td>
<td>osc</td>
</tr>
</tbody>
</table>

*Sat: saturated control output, Unsat: unsaturated control output, Osc: oscillatory response

From this study, it can be seen that there were mutual effect between α and ω. So, the step response cannot be evaluated from the value of α or ω alone. The best response was observed from A3 where this setting gave no overshoot, fastest settling time and no steady-state error under both conditions. The effect of actuator constraint towards controlled output can be observed for cases A2, A3, A7, A10, and A15. Figure 6 to 10 show the output response during unconstrained and constrained controller output for the respective cases.

The output responses show almost similar results when the controller output was saturated. This is shown in Figure 11. Therefore, optimal setting of poles location was made from the unconstrained condition where A3 satisfy the control requirements for this process.
Figure 5. Effect of poles location on the closed-loop response for cases A1, A2, A3, and A8

Figure 6. Case A2 for saturated and unsaturated control output

Figure 7. Case A3 for saturated and unsaturated control output
Figure 8. Case A7 for saturated and unsaturated control output

Figure 9. Case A10 for saturated and unsaturated control output

Figure 10. Case A15 for saturated and unsaturated control output
4.2. Effect of Sampling Time

The effect of sampling time selection for controller update was evaluated between 10 seconds and 20 seconds. Steam temperature possessed a slow varying dynamics caused by the transport delay and large time constant. It took few seconds for the process to react upon the control signal. From figure 2, it is obvious that the time constant of the process is
in the order of tenth of seconds. Based on researcher experimental experiences, sampling time of 10 seconds would be adequate to capture the changes in process dynamics. Sampling time faster than this will only caused chattering in control signal and jeopardized the system performance.

Figure 12 shows comparison between two sampling times; 10 seconds and 20 seconds. A2 and A10 have common poles setting but A2’s sampling time was 10 seconds while A10’s was 20 seconds. From the figure, A2 was updated more frequent compared to A10 and consequently had smaller settling time. The same condition was observed from A7 and A15 as shown in figure 13. Based on these observations, the sampling time for the self-tuning controller was set to 10 seconds.

5. Experimental Results

From simulation results, the optimal setting for self-tuning controller was finalized. The sampling time was set to 10 seconds, $\alpha = 0.5$ and $\omega = 0.1$. The computer-based control was implemented using MATLAB Simulink R2009a. Initial condition for the parameter estimation was set to $[0.01; 0.02; 0.03; 0.04]$ respectively. The controller was set to regulate the steam temperature at 85°C. Figure 14 shows the experimental steam temperature output that was regulated from room temperature. It took about 3000s for the steam to reach 50°C and gain its energy. The steam temperature respond as expected where there was no overshoot and the steam temperature was maintained at 85°C for the whole duration.

It is considered as normal in the real process to have some fluctuations in the output caused by external disturbances and uncertainties. The rule of thumb in process regulation is to maintain the controlled variable within ±2% boundary. This gave tolerance of ±2°C from the set point temperature. Figure 15 shows a closed-up view during the steady-state. Steam temperature fluctuates between 84°C to 86°C from the final temperature and within acceptable boundaries.

![Figure 14. Experimental output when set to A3 and steam temperature regulated at 85°C](image1.png)

![Figure 15. Steady-state response lies within ±2% output boundary](image2.png)
6. Conclusions

The self-tuning PID based on pole-placement method was adopted to regulate the steam temperature of a steam distillation essential oil extraction process. The controller cascaded four additional poles to the process plant to influence the closed-loop response. These poles tailored to the percentage overshoot and response speed requirements which is of utmost important in process control. Simulation study helped to determine the optimal setting of the poles. Experimental implementation on a real process proved that the self-tuning controller can regulate the steam temperature at a desired set point without temperature overshoot when the poles were set to 0.5 and 0.1 with 10 sec. sampling time.

ACKNOWLEDGEMENTS

This research is supported by UiTM Excellence Fund 600-RMI-ST-DANA-5/3/DST(43/2010) and Ministry of Higher Education fund (600-RMI-ST-FRGS 5/3/Fst (85/2010)). The authors would like to thank the Faculty of Electrical Engineering, UiTM for providing the facilities to conduct this research and for the financial supports throughout the process.

REFERENCES